

Robotics

Erwin M. Bakker | LIACS Media Lab

15-2 2021



Universiteit
Leiden

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Organization and Overview

Period: February 1st – May 10th 2021
Time: Tuesday 16.15 – 18.00
Place: <https://smart.newrow.com/#/room/qba-943>
Lecturer: Dr Erwin M. Bakker (erwin@liacs.nl)
Assistant: Erqian Tang

NB Register on Brightspace

Schedule:

1-2	Introduction and Overview
8-2	No Class (Dies)
15-2	Locomotion and Inverse Kinematics
22-2	Robotics Sensors and Image Processing
1-3	Yetiborg Introduction + SLAM Workshop I
8-3	Project Proposals (presentation by students)
15-3	Robotics Vision
22-3	Robotics Reinforcement Learning
29-3	Yetiborg Qualification + Robotics Reinforcement Learning Workshop II
5-4	No Class (Eastern)
12-4	Project Progress (presentations by students)
19-4	Yetiborg Challenge
26-4	Project Team Meetings
3-5	Project Team Meetings
10-5	Online Project Demos

Website: <http://liacs.leidenuniv.nl/~bakkerem2/robotics/>



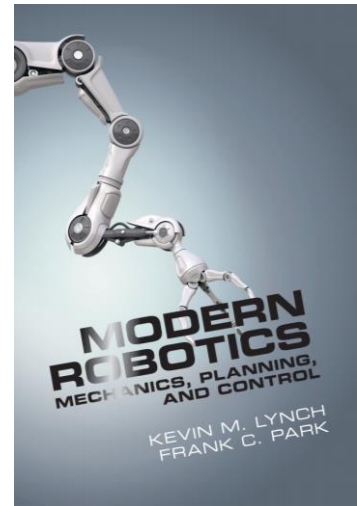
Grading (6 ECTS):

- Presentations and Robotics Project (60% of grade).
- Class discussions, attendance, workshops and assignments (40% of grade).
- It is necessary to be at every class and to complete every workshop.

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Overview

- Robotic Actuators
- Configuration Space
- Rigid Body Motion
- Forward Kinematics
- Inverse Kinematics
- Link: <http://modernrobotics.org>

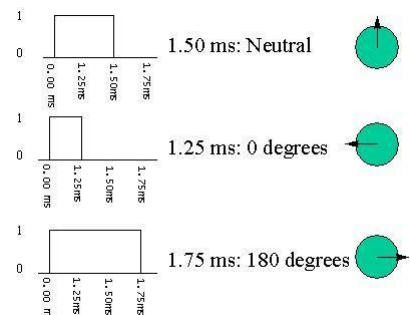
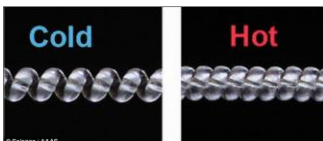


K.M. Lynch, F.C. Park, Modern Robotics: Mechanics, Planning and Control, Cambridge University Press, 2017

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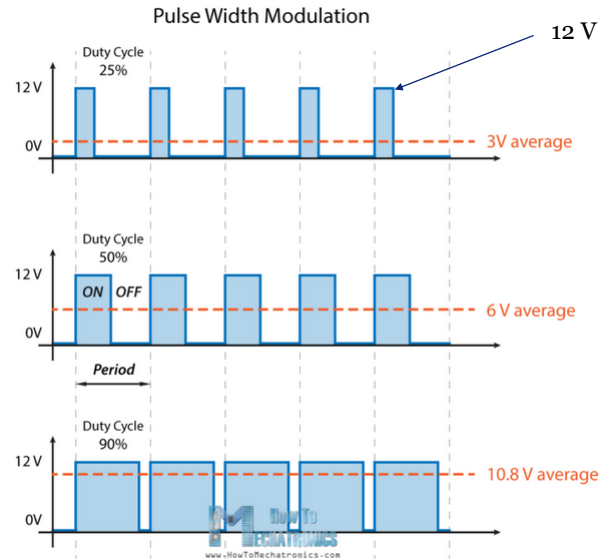
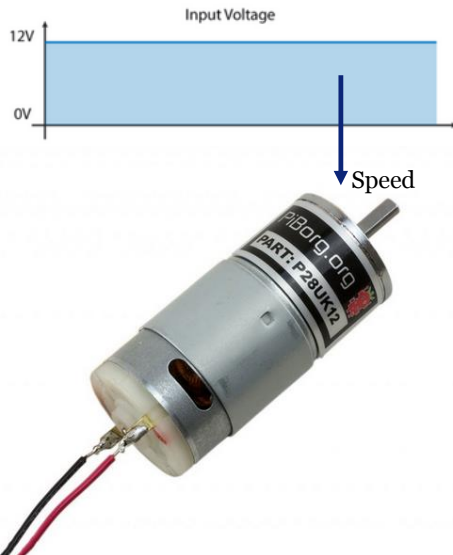
Robotics Actuators

- Electro motors
- Servo's
- Stepper Motors
- Brushless motors
- Solenoids
- Hydraulic, pneumatic actuator's
- Magnetic actuators
- Artificial Muscles
- Etc.



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DC Motors



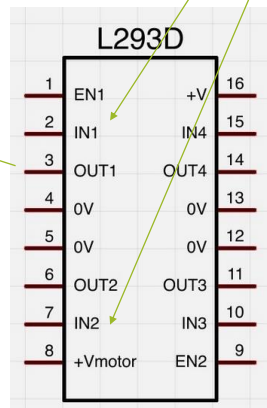
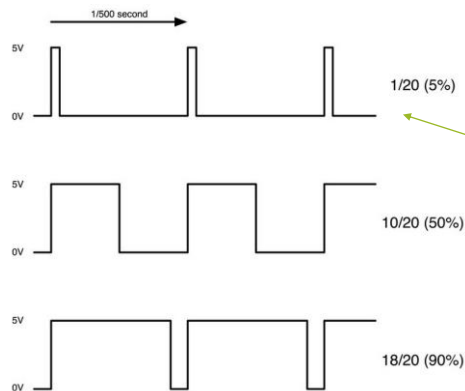
<https://howtomechanics.com/how-it-works/electronics/how-to-make-pwm-dc-motor-speed-controller-using-555-timer-ic/>

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DC Electro Motors:

- Duty Cycle

Brushed DC (BDC) motor driver



```
import RPi.GPIO as io
io.setmode(io.BCM)

in1_pin = 4
in2_pin = 17

io.setup(in1_pin, io.OUT)
io.setup(in2_pin, io.OUT)

def set(property, value):
    try:
        f = open("/sys/class/rpi-pwm/pwm0/" + property, "w")
        f.write(value)
        f.close()
    except:
        print("Error writing to: " + property + " value: " + value)

set("delayed", "0")
set("mode", "pwm")
set("frequency", "500")
set("active", "1")

def clockwise():
    io.output(in1_pin, True)
    io.output(in2_pin, False)

def counter_clockwise():
    io.output(in1_pin, False)
    io.output(in2_pin, True)

clockwise()










while True:
    cmd = raw_input("Command, f/r 0..9, E.g. f5 :")
    direction = cmd[0]
    if direction == "f":
        clockwise()
    else:
        counter_clockwise()
    speed = int(cmd[1]) * 11
    set("duty", str(speed))
```

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DC Motor Controllers

Pololu Simple Motor Controllers

- USB, TTL Serial, Analog, RC Control, I2C

	Original versions, not recommended for new designs (included for comparison purposes)					G2 versions, released November 2018			
									
Minimum operating voltage:	5.5 V	5.5 V	5.5 V	5.5 V	5.5 V	6.5 V	6.5 V	6.5 V	6.5 V
Recommended max operating voltage:	24 V(1)	24 V(1)	34 V(2)	24 V(1)	34 V(2)	24 V(1)	34 V(2)	24 V(1)	34 V(2)
Max nominal battery voltage:	18 V	18 V	28 V	18 V	28 V	18 V	28 V	18 V	28 V
Max continuous current (no additional cooling):	7 A	15 A	12 A	25 A	23 A	15 A	12 A	25 A	19 A
USB, TTL serial, Analog, RC control:	✓	✓	✓	✓	✓	✓	✓	✓	✓
I ² C control:						✓	✓	✓	✓
Hardware current limiting:						✓	✓	✓	✓
Reverse voltage protection:						✓	✓	✓	✓

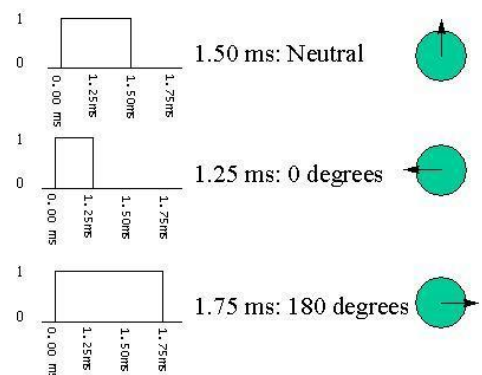
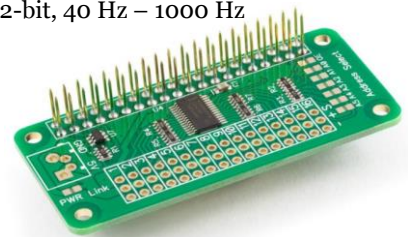
<https://www.pololu.com/category/94/pololu-simple-motor-controllers>

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Servo's



16-ch, 12-bit, 40 Hz – 1000 Hz

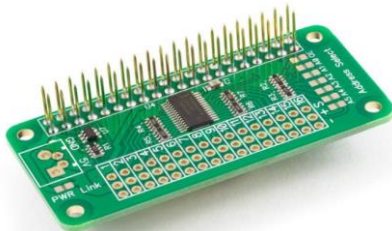


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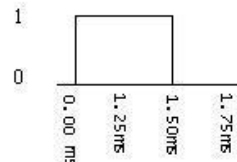
Servo's



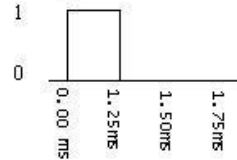
www.pololu.com



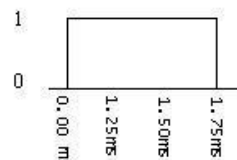
16-ch, 12-bit, 40 Hz – 1000 Hz



1.50 ms: Neutral



1.25 ms: 0 degrees



1.75 ms: 180 degrees

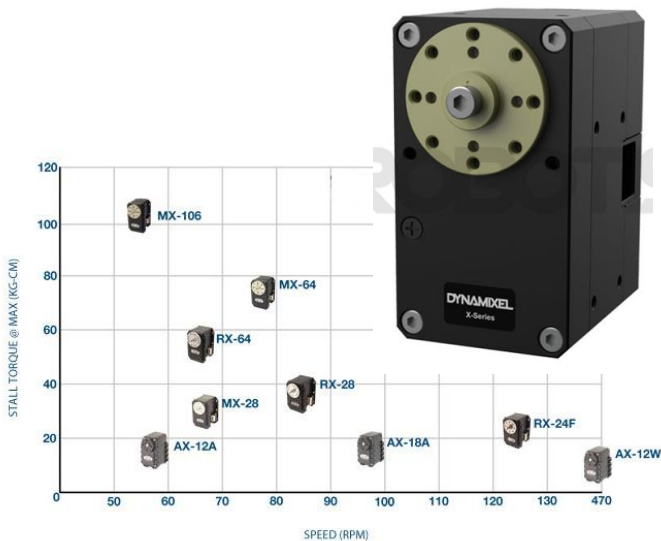
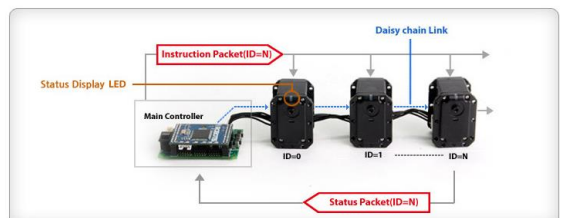
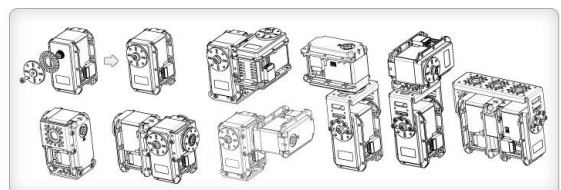


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Dynamixel Servo's



Flexible Construction and Modular Structures

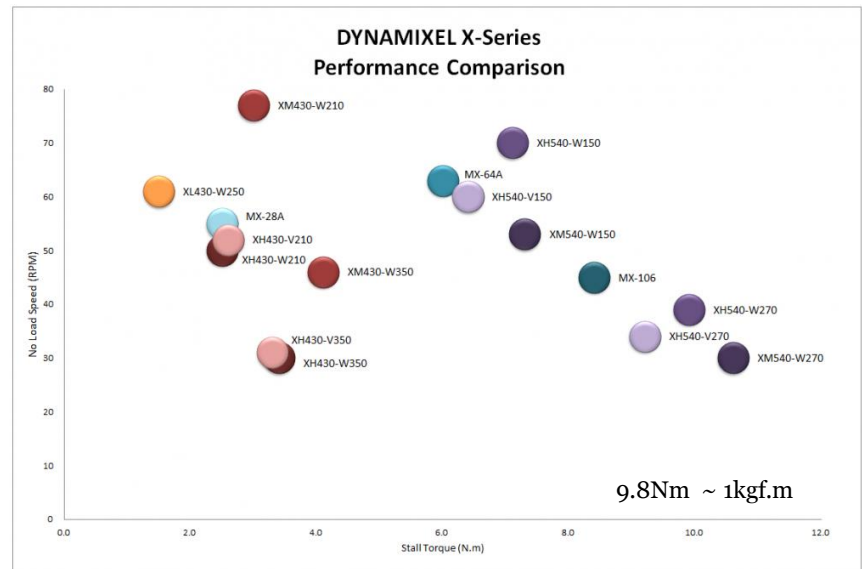


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Servo's



Performance Comparison



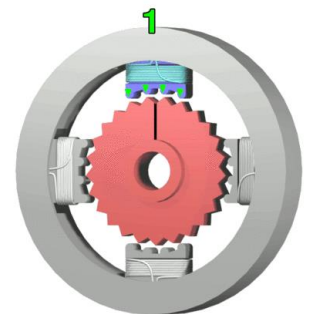
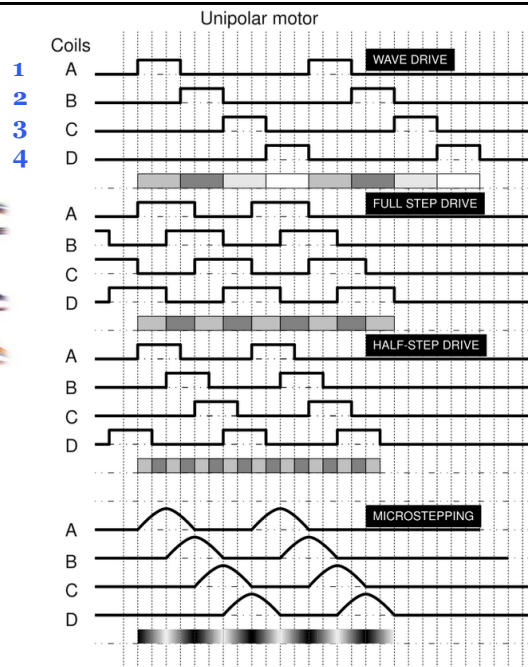
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Robotics Actuators



www.pololu.com

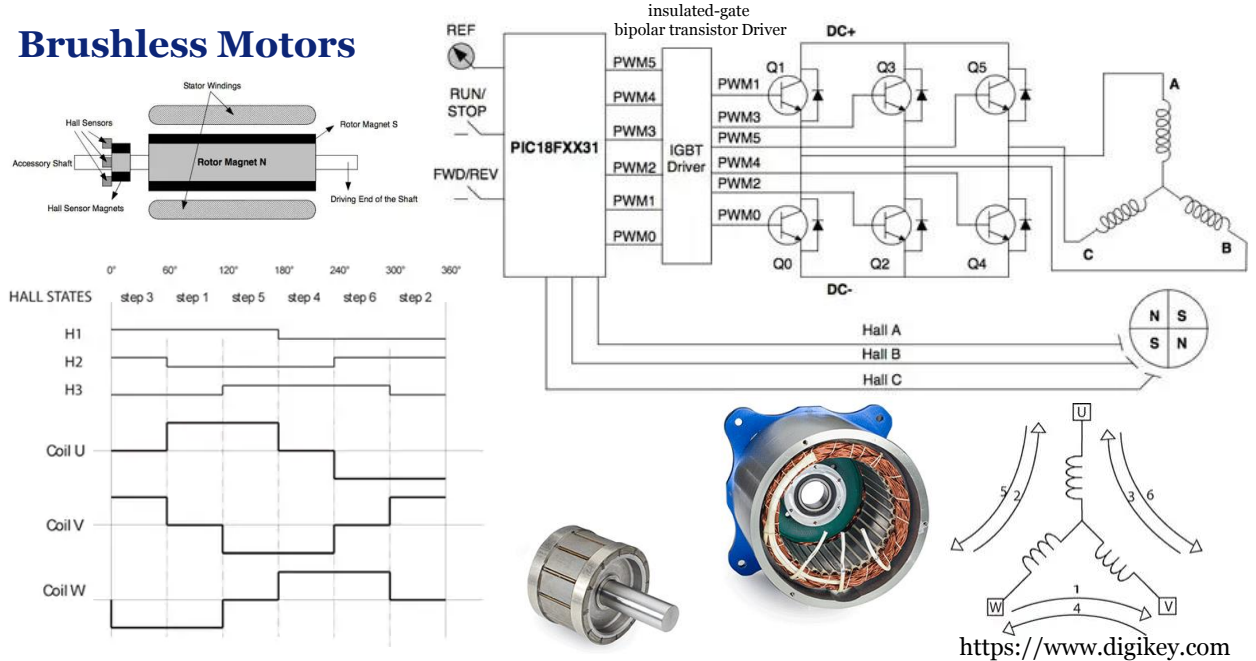
- Stepper motors
- Drivers: low-level, high level



By Wapcaplet; Teravolt. (Wikipedia)

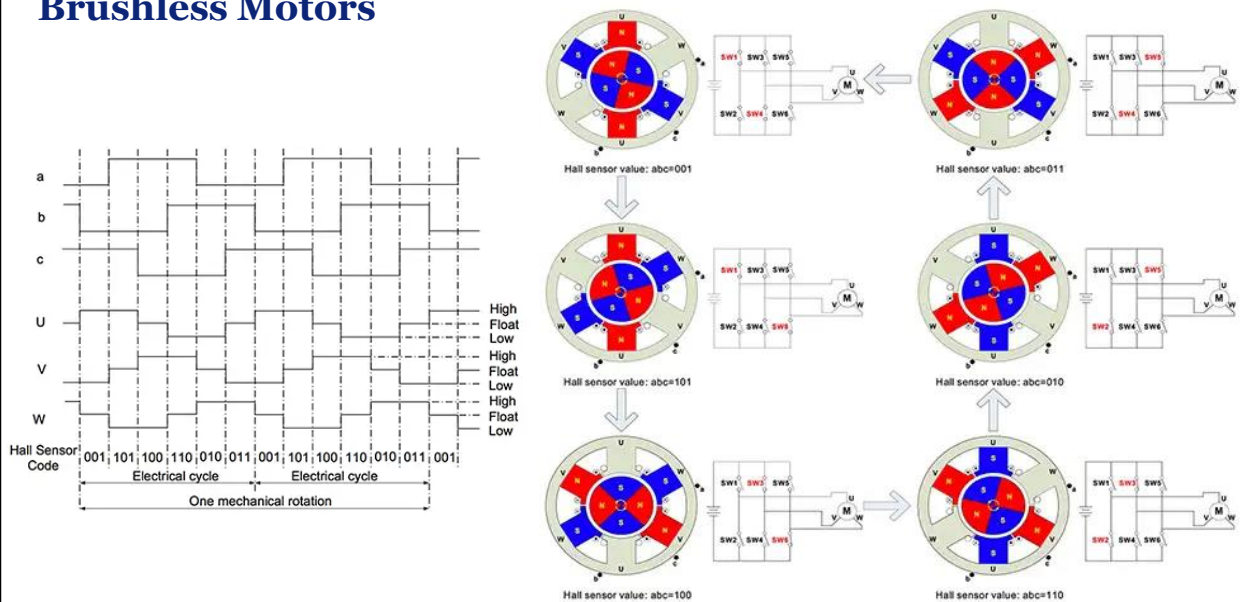
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Brushless Motors



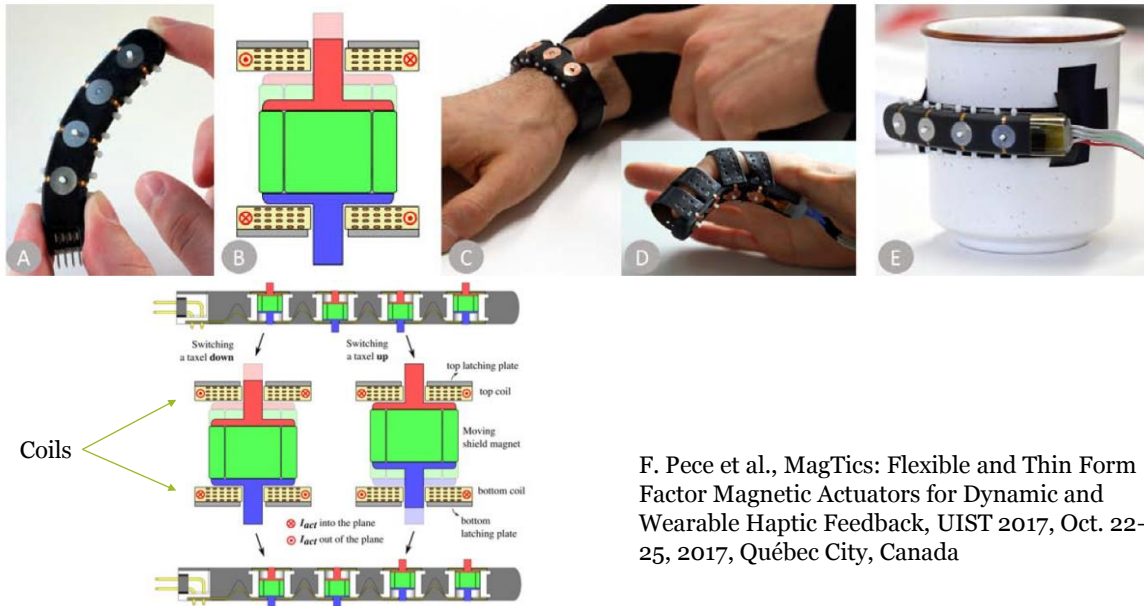
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Brushless Motors



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Flexible Magnetic Actuators



F. Pece et al., MagTics: Flexible and Thin Form Factor Magnetic Actuators for Dynamic and Wearable Haptic Feedback, UIST 2017, Oct. 22–25, 2017, Québec City, Canada

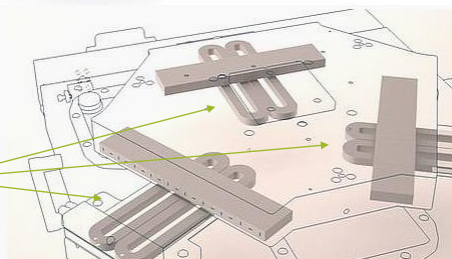
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Robotics Actuators

- 6D Magnetic Control
- <https://www.pi-usa.us>
- pimag-6d-magnetic-levitation

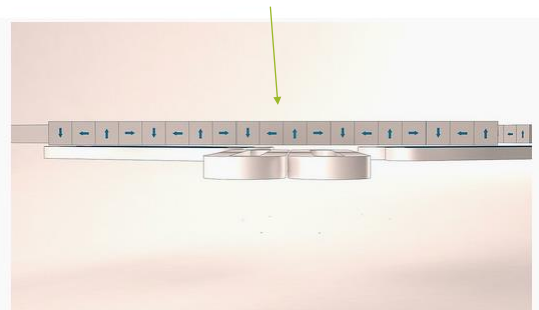


6 Coils



Simple structure: The platform levitates on a magnetic field generated by only six planar coils in the stator

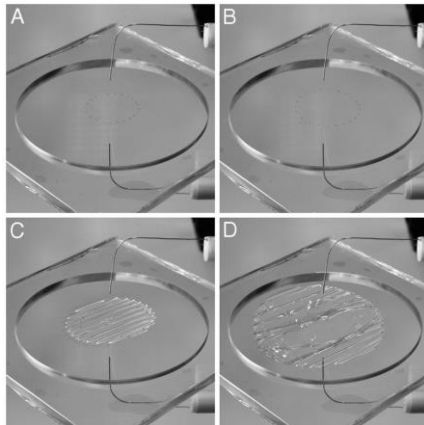
Halbach arrangement of magnets



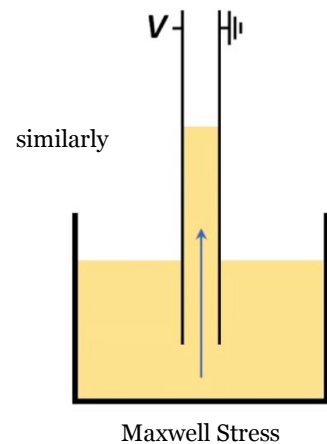
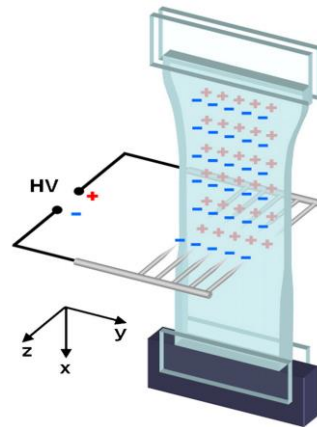
The Halbach arrangement of the magnets makes it possible, to minimize the energy required by the active coils in the stator for carrying the platform, to increase the load carrying capacity and to reduce thermal load

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Artificial Muscles



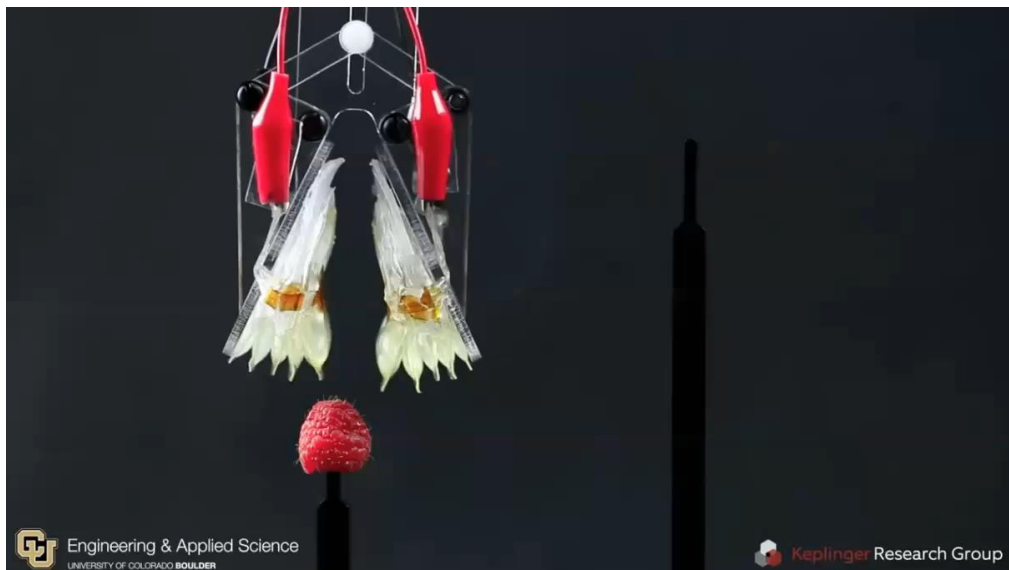
0 – 25 kV



Röntgen's electrode-free elastomer actuators without electromechanical pull-in instability by C. Keplinger, et al. PNAS March 9, 2010 107 (10) 4505-4510; <https://doi.org/10.1073/pnas.0913461107>

Röntgen WC (1880) Ueber die durch Electricität bewirkten Form—und Volumenänderungen von dielectrischen Körpern. Ann Phys Chem 11:771–786.

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See also TED Talk **The artificial muscles that will power robots of the future by Christoph Keplinger** <https://www.youtube.com/watch?v=ER15KmrB8h8>

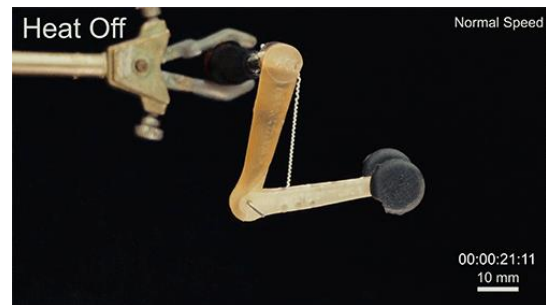
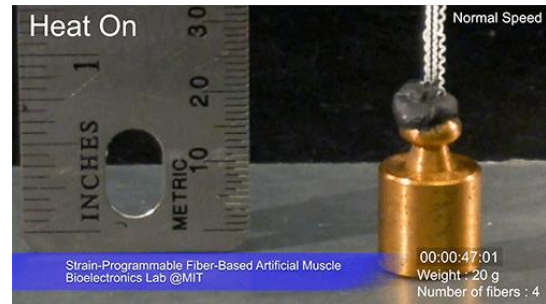
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MIT Artificial Muscles

- Combination of two dissimilar polymers into a single fiber
- The polymers have very different thermal expansion coefficients (as in bimetals)
- Developed by Mehmet Kanik, Sirma Örgüç, working with Polina Anikeeva, Yoel Fink, Anantha Chandrakasan, and C. Cem Taşan, and five others

<http://news.mit.edu/2019/artificial-fiber-muscles-0711>



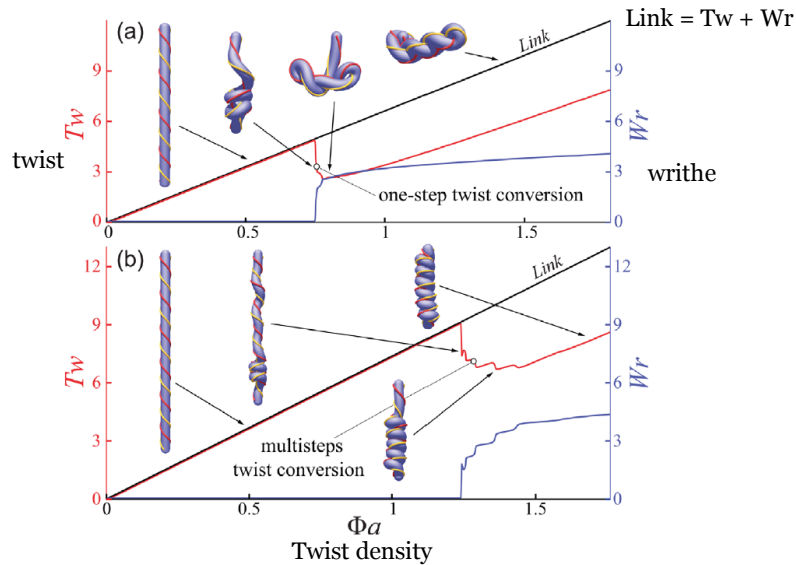
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Spanish Dancer by Micha Heilman and Stella Tsilia



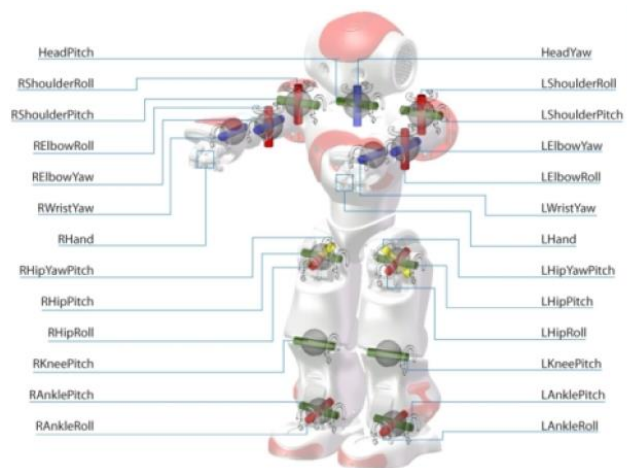
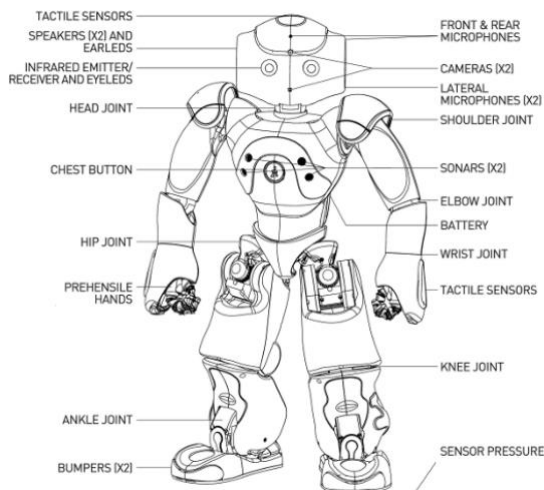
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N. Charles, M. Gazzola, and L. Mahadevan, **Topology, Geometry, and Mechanics of Strongly Stretched and Twisted Filaments: Solenoids, Plectonemes, and Artificial Muscle Fibers**
 PHYSICAL REVIEW LETTERS 123, 208003 (2019)



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NAO



http://doc.aldebaran.com/2-1/family/nao_dcm/actuator_sensor_names.html

Hexapod: S.P.I.N. by M. Huijben, M. Swenne, R. Voeter, S. Alvarez Rodriguez.

S.P.I.N. - Spider Python INator

Marcel Huijben (s1780107)
 Martijn Swenne (s1923889)
 Sebastiaan Alvarez Rodriguez (s1810979)
 Robin Voetter (s1835130)

2/15/2021

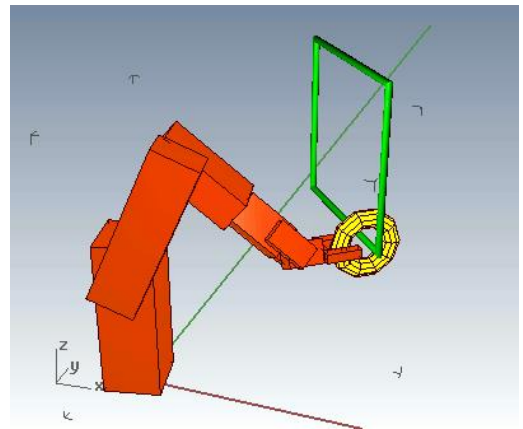
How to move to a goal?

Problem: How to move to a goal?

- Grasp, Walk, Stand, Dance, Follow, etc.

Solution:

1. *Program step by step*
 - *Computer Numerical Control (CNC), Automation.*
2. *Inverse kinematics:*
 - take end-points and move them to designated points.
3. *Tracing movements*
 - by specialist, human, etc.
4. ***Learn the right movements***
 - **Reinforcement Learning**, give a reward when the movement resembles the designated movement.



<https://pybullet.org/wordpress/>

Configuration Space

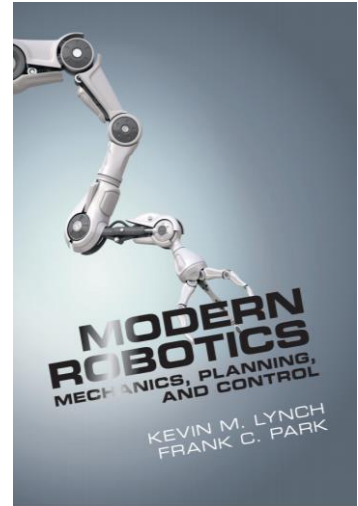
Robot Question: Where am I?

Answer:

The robot's configuration: a specification of the positions of all points of a robot.

Here we assume:

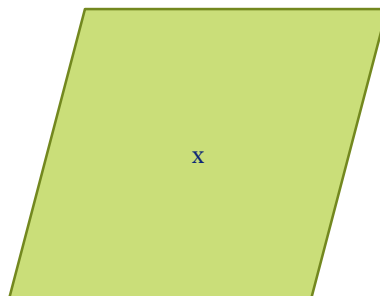
Robot links and bodies are rigid and of known shape => only a few variables needed to describe it's configuration.



K.M. Lynch, F.C. Park, Modern Robotics: Mechanics, Planning and Control, Cambridge University Press, 2017

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Configuration Space

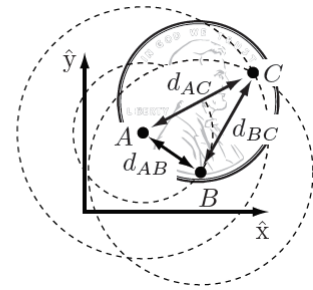


- Degrees of Freedom of a Rigid Body: the smallest number of real-valued coordinates needed to represent its configuration

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Configuration Space

Assume a coin (heads) with 3 points A, B, C on it.



In the plane A,B,C have 6 degrees of freedom: (x_A, y_A) , (x_B, y_B) , (x_C, y_C)

A coin is rigid \Rightarrow 3 extra constraints on distances: d_{AB} , d_{AC} , d_{BC}

These are fixed, wherever the location of the coin.

1. The coin and hence A can be placed everywhere $\Rightarrow (x_A, y_A)$ free to choose.
2. B can only be placed under the constraint that its distance to A would be equal to d_{AB} .
 \Rightarrow freedom to turn the coin around A with angle $\varphi_{AB} \Rightarrow (x_A, y_A, \varphi_{AB})$ are free to choose.
3. C should be placed at distance d_{AC} , d_{BC} from A and B, respectively
 \Rightarrow only 1 possibility, hence no degree of freedom added.

Degrees of Freedom (DOF) of a Coin

= sum of freedoms of the points – number of independent constraints

= number of variables – number of independent equations

$$= 6 - 3 = 3$$

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Configuration Space

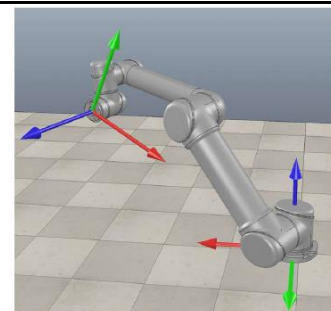
[1] Definition 2.1.

The **configuration** of a robot is a complete specification of the position of every point of the robot.

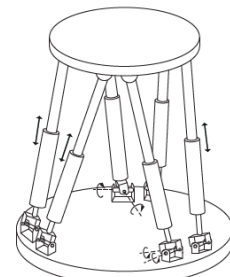
The minimum number n of real-valued coordinates needed to represent the configuration is the number of **degrees of freedom (dof)** of the robot.

The n -dimensional space containing all possible configurations of the robot is called the **Configuration Space (C-space)**.

The configuration of a robot is represented by a point in its C-space.



Open-chain robot: Manipulator (in V-REP). [1]



Closed-chain robot: Stewart-Gough platform. [1]

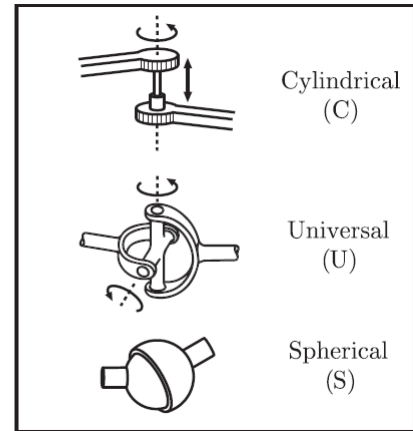
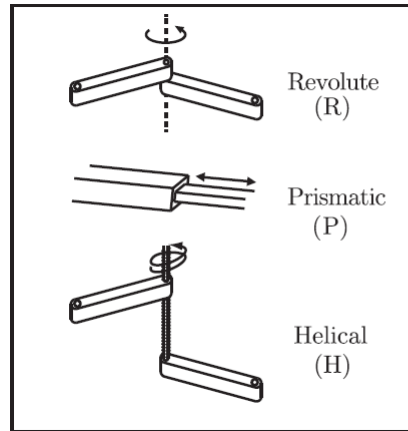
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Degrees of Freedom of a Robot

- A rigid body in 3D Space has **6 DOF**



- A joint can be seen to put constraints on the rigid bodies it connects
- It also allows freedom to move relative to the body it is attached to.



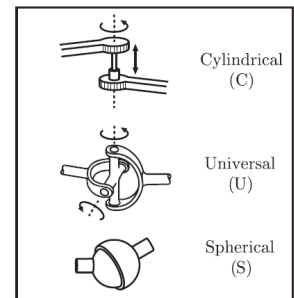
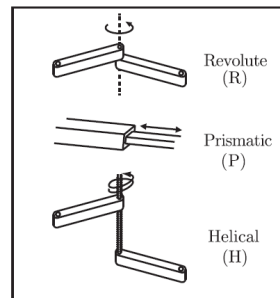
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Degrees of Freedom of a Robot

- A **rigid body** in 3D Space has 6 DOF



- A **joint** can be seen to put constraints on the rigid bodies it connects
- It also allows freedom to move relative to the body it is attached to.



Joint type	dof f	Constraints c between two planar rigid bodies	Constraints c between two spatial rigid bodies
Revolute (R)	1	2	5
Prismatic (P)	1	2	5
Helical (H)	1	N/A	5
Cylindrical (C)	2	N/A	4
Universal (U)	2	N/A	4
Spherical (S)	3	N/A	3

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Degrees of Freedom of a Robot

Proposition (Grübler's formula)

Consider a mechanism consisting of

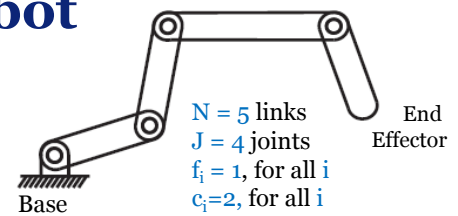
- N links, where ground is also regarded as a link.
- J number of joints,
- m number of degrees of freedom of a rigid body ($m = 3$ for planar mechanisms and $m = 6$ for spatial mechanisms),
- f_i the number of freedoms provided by joint i , and
- c_i the number of constraints provided by joint i , where $f_i + c_i = m$ for all i .

Then *Grübler's formula* for the number of degrees of freedom of the robot is

$$dof = m(N - 1) - \sum_{i=1}^J c_i = m(N - 1 - J) + \sum_{i=1}^J f_i$$

This formula holds only if all joint constraints are independent. If they are not independent then the formula provides a lower bound on the number of degrees of freedom.

Planar Mechanism DOF = 4



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Joint reactions in rigid body mechanisms with dependent constraints

Marek Wojtyra *

Warsaw University of Technology, Institute of Aeronautics and Applied Mechanics, ul. Nowowiejska 24, 00-665 Warsaw, Poland

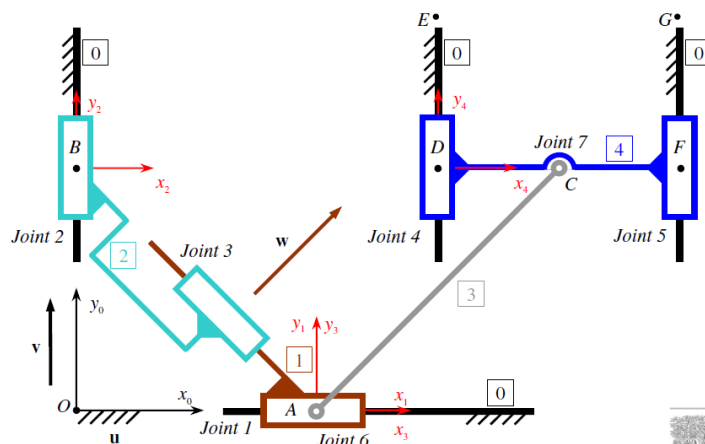


Fig. 1. Planar mechanism.

$$dof = m(N - 1) - \sum_{i=1}^J c_i = m(N - 1 - J) + \sum_{i=1}^J f_i$$

Mechanism and Machine Theory 44 (2009) 2265–2278

Contents lists available at ScienceDirect

Mechanism and Machine Theory

Journal homepage: www.elsevier.com/locate/mechmt



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Links

1

3

3

6

3

1

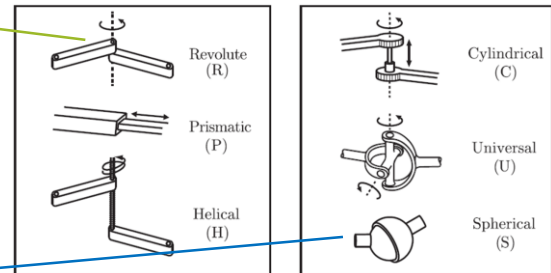
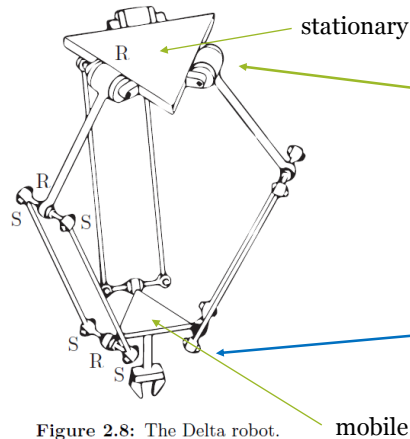


Figure 2.8: The Delta robot.

mobile

Example 2.7 (Delta robot). The Delta robot of Figure 2.8 consists of two platforms – the lower one mobile, the upper one stationary – connected by three legs. Each leg contains a parallelogram closed chain and consists of three revolute joints, four spherical joints, and five links. Adding the two platforms, there are $N = 17$ links and $J = 21$ joints (nine revolute and 12 spherical). By Grübler's formula,

$$\text{dof} = 6(17 - 1 - 21) + 9(1) + 12(3) = 15.$$

- Links: $1 + 3 + 3 + 6 + 3 + 1 = 17$
- Joints: $21: 9 \times R(1 \text{ dof})$ and $12 \times S(3 \text{ dof})$
- $m = 6$

$$\text{dof} = m(N - 1) - \sum_{i=1}^J c_i = m(N - 1 - J) + \sum_{i=1}^J f_i$$

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Systems and their Topologies

Note: $S^1 \times S^1 = T^2$ (not S^2)

Coordinates

Explicit Coordinates

- Euclidean (x, y)
- Polar (r, ϕ)
- Combined $(x, y) \times (r, \phi)$

Implicit Coordinates

- $\{(x, y, z) \mid x^2 + y^2 + z^2 = 1\}$

system	topology	sample representation
 point on a plane	 \mathbb{E}^2	 \mathbb{R}^2
 spherical pendulum	 S^2	 latitude 90° -180° -90° 180° longitude $[-180^\circ, 180^\circ] \times [-90^\circ, 90^\circ]$
 2R robot arm	 $T^2 = S^1 \times S^1$	 θ_2 2π 0 0 2π θ ₁ $[0, 2\pi) \times [0, 2\pi)$
 rotating sliding knob	 $\mathbb{E}^1 \times S^1$	 θ 2π 0 x $\mathbb{R}^1 \times [0, 2\pi)$

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C-Space (Configuration Space)

How to describe a rigid body's position and orientation in C-Space?

Fixed reference frame $\{s\}$

Reference frame attached to body $\{b\}$

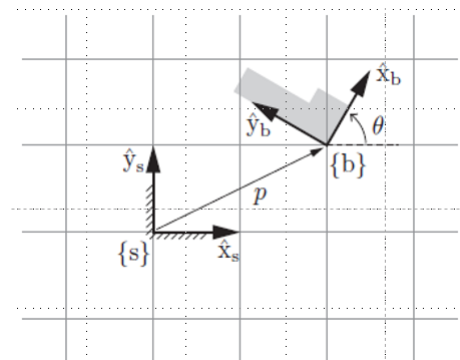
In \mathbb{R}^3 described by a 4×4 matrix with 10 constraints

(constraints, e.g.: unit-length, orthogonal)

Note: a point in $\mathbb{R}^3 \times S^2 \times S^1$

Matrix can be used to:

1. Translate or rotate a vector or a frame
2. Change the representation of a vector or a frame
 - for example from relative to $\{s\}$ to relative to $\{b\}$

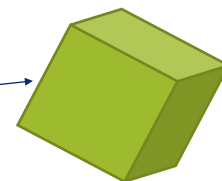
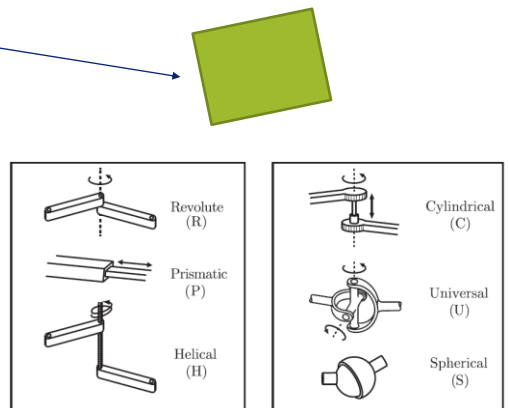


in the plane $\mathbb{R}^2 \times S^1$

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C-Spaces

- The C-space of a rigid body in the plane can be written as $\mathbb{R}^2 \times S^1$, since the configuration can be represented as the concatenation of the coordinates (x, y) representing \mathbb{R}^2 and an angle θ representing S^1 .
- The C-space of a PR robot arm can be written $\mathbb{R}^1 \times S^1$ (We will occasionally ignore joint limits, i.e., bounds on the travel of the joints, when expressing the topology of the C-space; with joint limits, the C-space is the Cartesian product of two closed intervals of the line.)
- The C-space of a 2R robot arm can be written $S^1 \times S^1 = T^2$, where T^n is the n -dimensional surface of a torus in an $(n+1)$ -dimensional space. (See Table 2.2.) Note that $S^1 \times S^1 \times \dots \times S^1$ (n copies of S^1) is equal to T^n , not S^n ; for example, a sphere S^2 is not topologically equivalent to a torus T^2 .
- The C-space of a planar rigid body (e.g., the chassis of a mobile robot) with a 2R robot arm can be written as $\mathbb{R}^2 \times S^1 \times T^2 = \mathbb{R}^2 \times T^3$
- As we saw in Section 2.1 when we counted the degrees of freedom of a rigid body in three dimensions, the configuration of a rigid body can be described by a point in \mathbb{R}^3 , plus a point on a two-dimensional sphere S^2 , plus a point on a one-dimensional circle S^1 , giving a total C-space of $\mathbb{R}^3 \times S^2 \times S^1$.



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Task Space and Work Space

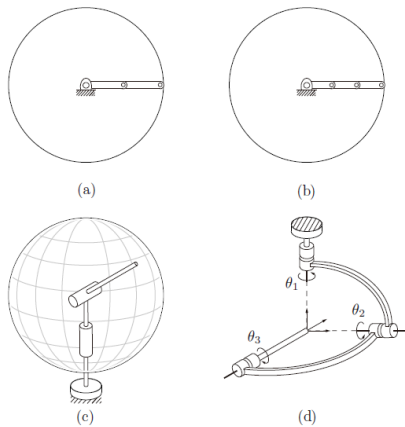
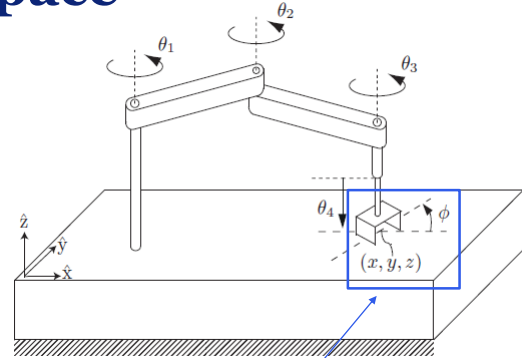


Figure 2.12: Examples of workspaces for various robots: (a) a planar 2R open chain; (b) a planar 3R open chain; (c) a spherical 2R open chain; (d) a 3R orienting mechanism.

The **workspace** is a specification of the configurations that the end-effector of the robot can reach.



The SCARA robot is an **RRRP open chain** that is widely used for tabletop pick-and-place tasks. The end-effector configuration is completely described by (x, y, z, ϕ)

⇒ **task space** $R^3 \times S^1$ and

⇒ **workspace** as the reachable points in (x, y, z) , since all orientations ϕ can be achieved at all reachable points.

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Rigid Body Motion

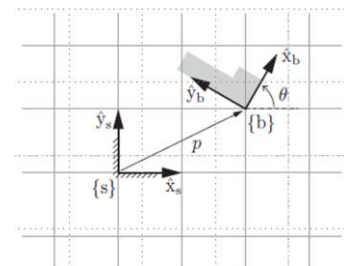
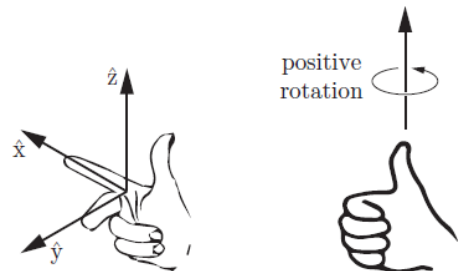
Rigid-body position and orientation $(x, y, z, \phi, \theta, \psi) \in \mathbb{R}^3 \times S^2 \times S^1$

- Can also be described by 4x4 matrix with 10 constraints.
- In general 4x4 matrices can be used for
 - Location
 - Translation + rotation of a vector or frame
 - Transformation of coordinates between frames
- Velocity of a rigid body: $(\partial x/\partial t, \partial y/\partial t, \partial z/\partial t, \partial \phi/\partial t, \partial \theta/\partial t, \partial \psi/\partial t)$

Exponential coordinates:

Every rigid-body configuration can be achieved by:

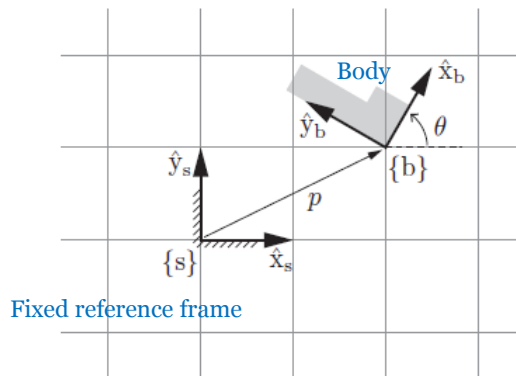
- Starting in the fixed home frame and integrating a constant twist for a specified time.
- Direction of a screw axis and scalar to indicate how far the screw axis must be followed



Similarly in the plane

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Rigid Body Motions in the Plane



$$p = p_x \hat{x}_s + p_y \hat{y}_s.$$

$$\hat{x}_b = \cos \theta \hat{x}_s + \sin \theta \hat{y}_s,$$

$$\hat{y}_b = -\sin \theta \hat{x}_s + \cos \theta \hat{y}_s.$$

Figure 3.3: The body frame $\{b\}$ is expressed in the fixed-frame coordinates $\{s\}$ by the vector p and the directions of the unit axes \hat{x}_b and \hat{y}_b . In this example, $p = (2, 1)$ and $\theta = 60^\circ$, so $\hat{x}_b = (\cos \theta, \sin \theta) = (0.5, 1/\sqrt{2})$ and $\hat{y}_b = (-\sin \theta, \cos \theta) = (-1/\sqrt{2}, 0.5)$.

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Rigid Body Motions in the Plane

Previously:

$$p = p_x \hat{x}_s + p_y \hat{y}_s.$$

$$\hat{x}_b = \cos \theta \hat{x}_s + \sin \theta \hat{y}_s,$$

$$\hat{y}_b = -\sin \theta \hat{x}_s + \cos \theta \hat{y}_s.$$

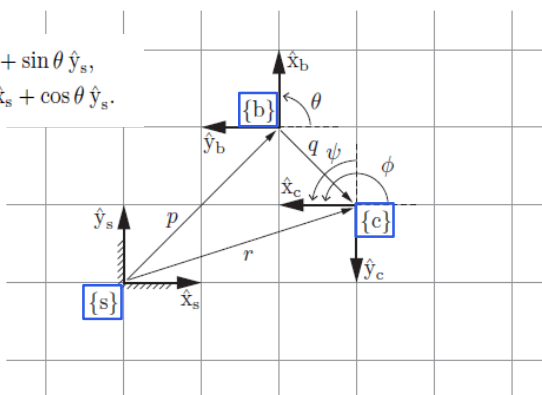


Figure 3.4: The frame $\{b\}$ in $\{s\}$ is given by (P, p) , and the frame $\{c\}$ in $\{b\}$ is given by (Q, q) . From these we can derive the frame $\{c\}$ in $\{s\}$, described by (R, r) . The numerical values of the vectors p , q , and r and the coordinate-axis directions of the three frames are evident from the grid of unit squares.

$\{b\}$ relative to $\{s\}$

$$p = \begin{bmatrix} p_x \\ p_y \end{bmatrix}$$

$$P = [\hat{x}_b \ \hat{y}_b] = \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix}$$

$\{c\}$ relative to $\{b\}$

$$q = \begin{bmatrix} q_x \\ q_y \end{bmatrix}, \quad Q = \begin{bmatrix} \cos \psi & -\sin \psi \\ \sin \psi & \cos \psi \end{bmatrix}$$



$\{c\}$ relative to $\{s\}$

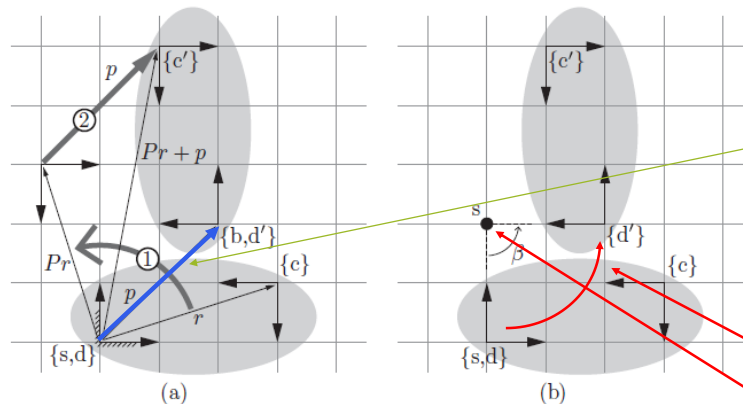
$$r = \begin{bmatrix} r_x \\ r_y \end{bmatrix}, \quad R = \begin{bmatrix} \cos \phi & -\sin \phi \\ \sin \phi & \cos \phi \end{bmatrix}$$

Note and verify:

$$R = PQ, \text{ and } r = Pq + p$$

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Rigid Body Motions in the Plane



(P, p) can be used to

1. Represent a configuration of a rigid body in {s}
2. Change the reference frame for vector representation.
3. **Displace a vector or a frame.**

{c} described by (R,r)

$$r = \begin{bmatrix} r_x \\ r_y \end{bmatrix}, \quad R = \begin{bmatrix} \cos \phi & -\sin \phi \\ \sin \phi & \cos \phi \end{bmatrix}$$

Move rigid body such that {d} coincides with {d'}.

$$p = \begin{bmatrix} p_x \\ p_y \end{bmatrix} \quad P = [\hat{x}_b \ \hat{y}_b] = \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix}$$

Then {c'} described by (R',r'):

$$R' = PR, \\ r' = Pr + p,$$

Note: **SCREW MOTION**

The above **rotation** followed by a **translation** can also be expressed as

a rotation of the rigid-body about a fixed point s by an angle β

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Rigid Body Motions in the Plane

Note: **SCREW MOTION**

The above rotation followed by a translation can also be expressed as a rotation of the rigid-body about a fixed point s by an angle β

(β, s_x, s_y), where (s_x, s_y) = (0, 2)

In the {s}-frame rotate 1 rad/sec with speed (v_x, v_y) = (2, 0) is denoted as:

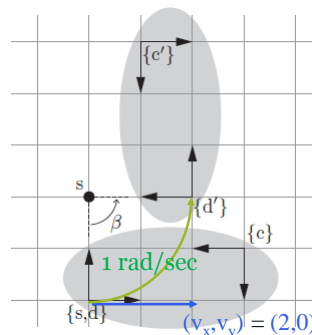
$$S = (\omega, v_x, v_y) = (1, 2, 0)$$

Following the screw-axis for an angle

$\theta = \pi/2$ gives the displacement we want:

$$S\theta = (\pi/2, \pi, 0)$$

These are called the **exponential coordinates** for the planar rigid-body displacement.



{c} described by (R,r)

$$r = \begin{bmatrix} r_x \\ r_y \end{bmatrix}, \quad R = \begin{bmatrix} \cos \phi & -\sin \phi \\ \sin \phi & \cos \phi \end{bmatrix}$$

Move rigid body such that {d} coincides with {d'}.

$$p = \begin{bmatrix} p_x \\ p_y \end{bmatrix} \quad P = [\hat{x}_b \ \hat{y}_b] = \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix}$$

Then {c'} described by (R',r'):

$$R' = PR, \\ r' = Pr + p,$$

Note:

- distance = vt

- distance along quarter circle with radius 2 equals π .

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Forward Kinematics

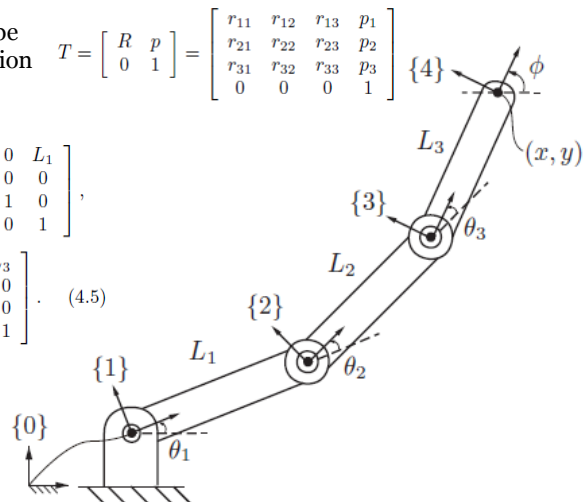
The forward kinematics of 3R Planar Open Chain can be written as a product of four homogeneous transformation matrices: $T_{04} = T_{01}T_{12}T_{23}T_{34}$, where

$$T_{01} = \begin{bmatrix} \cos \theta_1 & -\sin \theta_1 & 0 & 0 \\ \sin \theta_1 & \cos \theta_1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, \quad T_{12} = \begin{bmatrix} \cos \theta_2 & -\sin \theta_2 & 0 & L_1 \\ \sin \theta_2 & \cos \theta_2 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix},$$

$$T_{23} = \begin{bmatrix} \cos \theta_3 & -\sin \theta_3 & 0 & L_2 \\ \sin \theta_3 & \cos \theta_3 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, \quad T_{34} = \begin{bmatrix} 1 & 0 & 0 & L_3 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}. \quad (4.5)$$

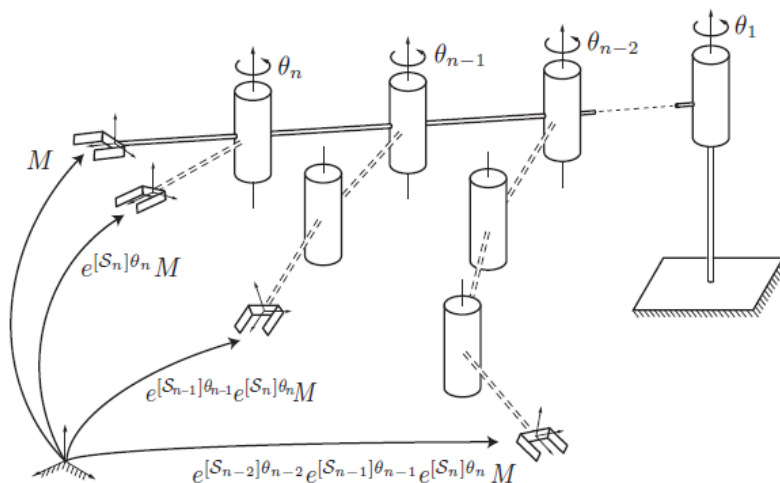
Home position M:

$$M = \begin{bmatrix} 1 & 0 & 0 & L_1 + L_2 + L_3 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



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Forward Kinematics: Product of Exponentials



PoE parameters also known as Euler-Rodrigues parameters.

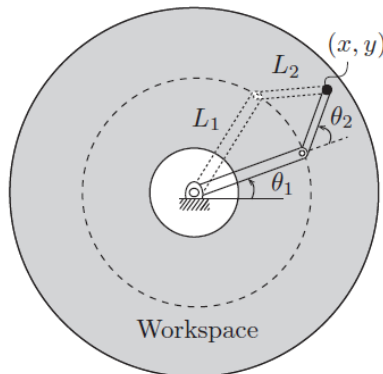
There are many other representations:
- for example Denavit-Hartenberg (1955) representation is very popular, but can be cumbersome

In velocity kinematics Jacobians are used.

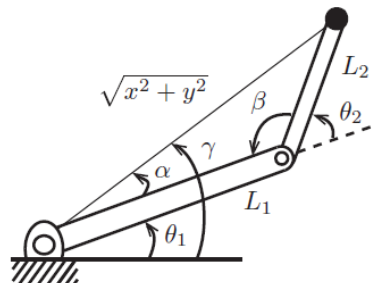
Figure 4.2: Illustration of the PoE formula for an n -link spatial open chain.

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Inverse Kinematics Which angles θ_1 , and θ_2 will lead to location (x,y) ?



(a) A workspace, and lefty and righty configurations.



(b) Geometric solution.

Law of cosines gives:

$$L_1^2 + L_2^2 - 2L_1L_2 \cos \beta = x^2 + y^2$$

, hence

$$\beta = \cos^{-1} \left(\frac{L_1^2 + L_2^2 - x^2 - y^2}{2L_1L_2} \right)$$

,and similarly

$$\alpha = \cos^{-1} \left(\frac{x^2 + y^2 + L_1^2 - L_2^2}{2L_1 \sqrt{x^2 + y^2}} \right)$$

$$\gamma = \text{atan2}(y, x)$$

Answer:

$$\theta_1 = \gamma - \alpha, \quad \theta_2 = \pi - \beta$$

Figure 6.1: Inverse kinematics of a 2R planar open chain.

In general: IK-Solvers, Newton-Raphson, etc.

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Real Time Physics Modelling

<https://pybullet.org/wordpress/>

pybullet KUKA
grasp training

Using Tensorflow
OpenAI gym
Baselines
DeepQNetworks (DQNs)

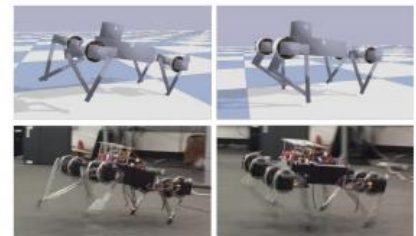
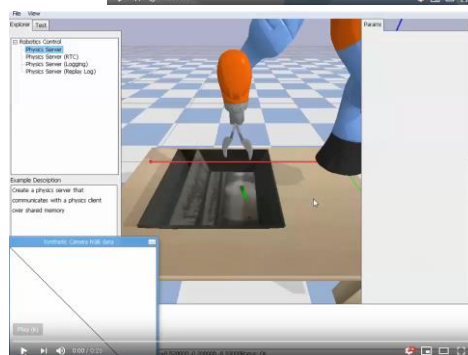
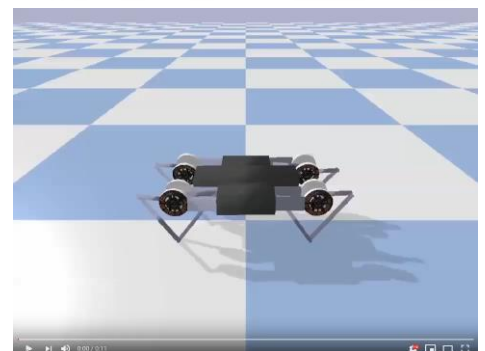


Fig. 1: The simulated and the real Minitaurs learned to gallop using deep reinforcement learning.



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Organization and Overview

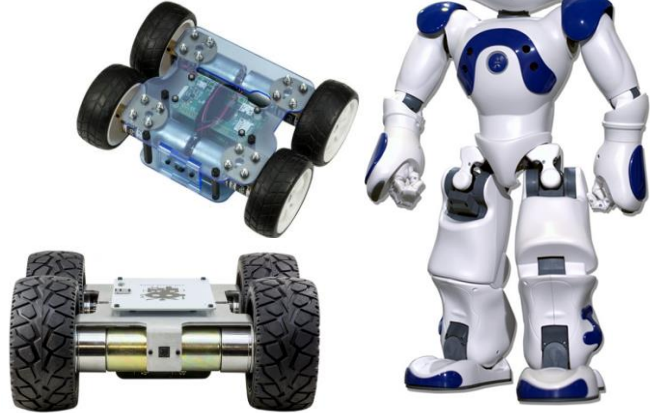
Period: February 1st – May 10th 2021
Time: Tuesday 16.15 – 18.00
Place: <https://smart.newrow.com/#/room/qba-943>
Lecturer: Dr Erwin M. Bakker (erwin@liacs.nl)
Assistant: Erqian Tang

NB Register on Brightspace

Schedule:

1-2	Introduction and Overview
8-2	No Class (Dies)
15-2	Locomotion and Inverse Kinematics
22-2	Robotics Sensors and Image Processing
1-3	Yetiborg Introduction + SLAM Workshop I
8-3	Project Proposals (presentation by students)
15-3	Robotics Vision
22-3	Robotics Reinforcement Learning
29-3	Yetiborg Qualification + Robotics Reinforcement Learning Workshop II
5-4	No Class (Eastern)
12-4	Project Progress (presentations by students)
19-4	Yetiborg Challenge
26-4	Project Team Meetings
3-5	Project Team Meetings
10-5	Online Project Demos

Website: <http://liacs.leidenuniv.nl/~bakkerem2/robotics/>



Grading (6 ECTS):

- Presentations and Robotics Project (60% of grade).
- Class discussions, attendance, workshops and assignments (40% of grade).
- It is necessary to be at every class and to complete every workshop.

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Robotics Homework II

Visit <http://modernrobotics.org> and obtain the pdf of the [book](#).

Read Chapters 1 and 2 and answer the following exercises:

- 2.2
- 2.10 for Figures 2.19 a, and b
- 2.19

Due: Monday 22-2 at 14.00 PM.

Email your answers to erwin@liacs.nl with subject 'Robotics2021 HW2'.

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References

1. K.M. Lynch, F.C. Park, Modern Robotics: Mechanics, Planning and Control, Cambridge University Press, 2017. (DOI: 10.1017/97813166661239)
2. <https://pybullet.org/wordpress/>